

# SPIT MULTI-MAX

Zinc coated & stainless steel



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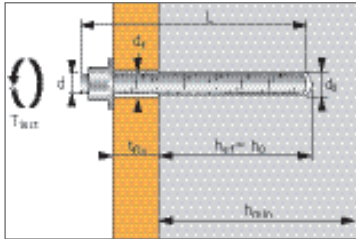
ETA Option 7 Methacrylate chemical resin  
n° 13/0435

## Technical data

MULTI-MAX Resin with threaded rods	Max. anchor depth (mm)	Max. thick of base material (mm)	Ø thread (mm)	Drilling depth (mm)	Ø Drill bit (mm)	Ø Clearance (mm)	Total rod length (mm)	Max. tighten (Nm)
	$h_{ef}$	$h_{min}$	$d$	$h_o$	$d_o$	$d_f$	$L$	$T_{inst}$
Rod M8	80	110	8	80	10	9	110	10
Rod M10	90	120	10	90	12	12	130	20
Rod M12	110	140	12	110	14	14	160	30
Rod M16	125	160	16	128	18	18	190	60
Rod M20	170	220	20	170	25	22	260	120
Rod M24	210	265	24	210	28	26	300	200

MULTI-MAX: Dual component cartridge methacrylate resin - vol. 280 ml  
- vol. 410 ml

Code 060040  
Code 060047



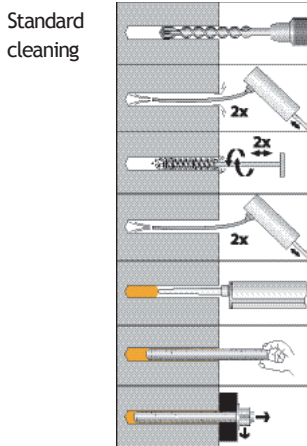
## APPLICATION

- Fixing steel framed structures
- Fixing machinery (resistant to vibration)
- Fixing of storage silos, refinery pipework supports
- Fixing motorway signs
- Fixing safety barriers

## MATERIAL

- **Threaded rod M8-M16:**  
cold formed steel NF A35-053
- **Threaded rod M20-M30:**  
11 SMnPb37 - NFA 35-561
- **Nut:**  
Steel, EN 20898-2 grade 6 or 8
- **Washer:**  
Steel DIN 513
- **Zinc coating 5 µm min.**  
NF E25-009

## INSTALLATION



## Anchor mechanical properties

Threaded part (maxima Rod)	M8	M10	M12	M16	M20	M24
$f_{uk}$ (N/mm <sup>2</sup> ) Min. tensile strength	600	600	600	600	520	520
$f_{yk}$ (N/mm <sup>2</sup> ) Yield strength	420	420	420	420	420	420
$A_s$ (mm <sup>2</sup> ) Stressed cross-section	36,6	58	84,3	157	227	326,9
$W_{el}$ (mm <sup>3</sup> ) Elastic section modulus	31,2	62,3	109,2	277,5	482,4	833,7
$M^{0}_{Rk,s}$ (Nm) Characteristic bending moment	22	45	78	200	301	520
$M$ (Nm) Recommended bending moment	9,0	18,4	31,8	81,6	122,9	212,2

## Working time and curing time

Ambient temperature (°C)	Working time	Curing time
30°C > T ≥ 40°C	2 min	35 min
20°C > T ≥ 30°C	4 min	45 min
10°C > T ≥ 20°C	6 min	60 min
5°C > T ≥ 10°C	12 min	90 min
0°C > T ≥ 5°C	18 min	180 min
-5°C > T ≥ 0°C	-	360 min

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The loads specified on this page allow judging the product's performances, but cannot be used for the designing. The data given in the pages "CC method" have to be applied.

## Number of sealings per cartridge

Studs diameter	M8	M10	M12	M16	M20	M24
Drilling Ø (mm)	10	12	14	18	25	28
Drilling depth (mm)	80	90	110	125	170	210
<b>Nb. of sealings for one cartridge</b>						
MULTIMAX 280	103	75	52	35	8	7
MULTIMAX 410	151	110	76	51	12	10

## Ultimate ( $N_{Ru,m}$ , $V_{Ru,m}$ ) / characteristic loads ( $N_{Rk}$ , $V_{Rk}$ ) in kN

Mean Ultimate loads are derived from test results in admissible service conditions, and characteristic loads are statistically determined.

### TENSILE

Anchor size	M8	M10	M12	M16	M20	M24
$h_{ef}$	80	90	110	125	170	210
$N_{Ru,m}$	21,1	29,6	41,1	58,5	99,5	138,3
$N_{Rk}$	18,1	25,4	35,2	50,3	85,5	118,8

### SHEAR

Anchor size	M8	M10	M12	M16	M20	M24
$V_{Ru,m}$	15,92	22,75	32,8	56,2	73,6	115,0
$V_{Rk}$	10,98	18,9	25,3	46,8	59,02	95,8

## Design Loads ( $N_{Rd}$ , $V_{Rd}$ ) for one anchor without edge or spacing influence in kN

$$N_{Rd} = \frac{N_{Rk}^*}{\gamma_{Mc}}$$

\*Derived from test results

$$V_{Rd} = \frac{V_{Rk}^*}{\gamma_{Ms}}$$

### TENSILE

Anchor size	M8	M10	M12	M16	M20	M24
$h_{ef}$	80	90	110	125	170	210
$N_{Rd}$	12,1	14,1	19,6	27,9	47,5	66,0

$\gamma_{Mc} = 1,5$  for M8 &  $\gamma_{Mc} = 1,8$  for M10 to M24

### SHEAR

Anchor size	M8	M10	M12	M16	M20	M24
$V_{Rd}$	7,7	13,2	17,7	32,7	39,3	63,9

$\gamma_{Ms} = 1,43$  for M8 to M16 &  $\gamma_{Ms} = 1,5$  for M20 to M24

## Recommended loads ( $N_{Rec}$ , $V_{Rec}$ ) for one anchor without edge or spacing influence in kN

$$N_{Rec} = \frac{N_{Rk}^*}{\gamma_M \cdot \gamma_F}$$

\*Derived from test results

$$V_{Rec} = \frac{V_{Rk}^*}{\gamma_M \cdot \gamma_F}$$

### TENSILE

Anchor size	M8	M10	M12	M16	M20	M24
$h_{ef}$	80	90	110	125	170	210
$N_{Rec}$	8,6	10,1	14,0	19,9	33,9	47,1

$\gamma_F = 1,4$   
 $\gamma_{Mc} = 1,5$  for M8 &  $\gamma_{Mc} = 1,8$  for M10 to M24

### SHEAR

Anchor size	M8	M10	M12	M16	M20	M24
$V_{Rec}$	5,5	9,4	12,6	23,4	28,1	45,6

$\gamma_F = 1,4$   
 $\gamma_{Ms} = 1,43$  for M8 to M16 &  $\gamma_{Ms} = 1,5$  for M20 to M24

# SPIT MULTI-MAX

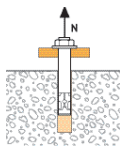
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## SPIT CC- Method (values issued from ETA)

### TENSILE in kN

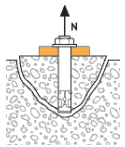


→ Pull out resistance for dry, wet (1) concrete

$$N_{Rd,p} = N_{Rd,p}^O \cdot f_b$$

Anchor size	Design pull-out resistance					
	M8	M10	M12	M16	M20	M24
$N_{Rd,p}^O$						
$h_{ef}$	80	90	110	125	170	210
-40 °C to +40 °C	12,1	14,1	19,6	27,9	47,5	66,0

$\gamma_{Mc} = 1,5$  for M8 &  $\gamma_{Mc} = 1,8$  for M10 to M24

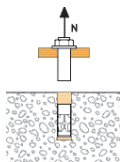


→ Concrete cone resistance for dry, wet (1) concrete

$$N_{Rd,c} = N_{Rd,c}^O \cdot f_b \cdot \Psi_s \cdot \Psi_{c,N}$$

Anchor size	Design cone resistance					
	M8	M10	M12	M16	M20	M24
$N_{Rd,c}^O$						
$h_{ef}$	80	90	110	125	170	210
-40 °C to +40 °C	24,0	23,9	32,3	39,1	62,1	85,2

$\gamma_{Mc} = 1,5$  for M8 &  $\gamma_{Mc} = 1,8$  for M10 to M24



→ Steel resistance

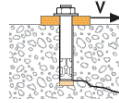
Anchor size	Steel design tensile resistance					
	M8	M10	M12	M16	M20	M24
Std. rod grade 5.8*	12,0	19,3	28,0	52,0	81,3	118,0
Std. rod grade 8.8*	19,3	30,7	44,7	84,0	130,7	188,0
Std. rod grade 10.9*	26,4	41,4	60,0	112,1	175,0	252,1
Std. rod grade A4*	13,7	21,7	31,6	58,8	91,7	132,1

Std. rod grade 5.8 & 8.8 :  $\gamma_{Ms} = 1,5$   
Std. rod grade 10.9 :  $\gamma_{Ms} = 1,4$   
Std. rod grade A4 :  $\gamma_{Ms} = 1,87$

$$N_{Rd} = \min(N_{Rd,p} ; N_{Rd,c} ; N_{Rd,s})$$

$$\beta_N = N_{Sd} / N_{Rd} \leq 1$$

### Shear in kN

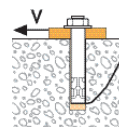


→ Concrete edge resistance

$$V_{Rd,c} = V_{Rd,c}^O \cdot f_b \cdot f_{\beta,V} \cdot \Psi_{S-C,V}$$

Anchor size	Design concrete edge resistance at minimum edge distance ( $C_{min}$ )					
	M8	M10	M12	M16	M20	M24
$V_{Rd,c}^O$						
$h_{ef}$	80	90	110	125	170	210
$C_{min}$	40	50	60	80	100	120
$S_{min}$	40	50	60	80	100	120
$V_{Rd,c}^O$	2,5	3,8	5,5	9,4	15,4	21,9

$\gamma_{Mc} = 1,5$

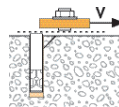


→ Pryout failure

$$V_{Rd,cp} = V_{Rd,cp}^O \cdot f_b \cdot \Psi_s \cdot \Psi_{c,N}$$

Anchor size	Design pryout resistance					
	M8	M10	M12	M16	M20	M24
$V_{Rd,cp}^O$						
$h_{ef}$	80	90	110	125	170	210
-40 °C to +40 °C	24,1	33,9	47,0	67,0	113,9	158,3

$\gamma_{Mcp} = 1,5$



→ Steel resistance

Anchor size	Steel design tensile resistance					
	M8	M10	M12	M16	M20	M24
Std. rod grade 5.8*	7,36	11,6	16,9	31,2	48,8	70,4
Std. rod grade 8.8*	11,68	18,6	27,0	50,4	78,4	112,8
Std. rod grade 10.9*	12,2	19,3	28,1	52,0	81,3	117,3
Std. rod grade A4*	7,3	11,9	17,3	32,7	51,3	73,1

Std. rod grade 5.8 et 8.8 :  $\gamma_{Ms} = 1,25$   
Std. rod grade 10.9 :  $\gamma_{Ms} = 1,5$   
Std. rod grade A4 :  $\gamma_{Ms} = 1,56$

\* Special grade available on request.

(1) Category 1

$$V_{Rd} = \min(V_{Rd,c} ; V_{Rd,cp} ; V_{Rd,s})$$

$$\beta_V = V_{Sd} / V_{Rd} \leq 1$$

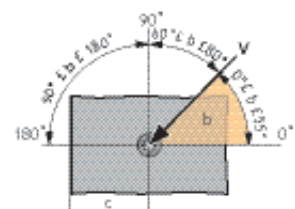
$$\beta_N + \beta_V \leq 1,2$$

### $f_B$ INFLUENCE OF CONCRETE

Concrete class	$f_B$
C25/30	1,02
C30/37	1,04
C40/50	1,07
C50/60	1,09

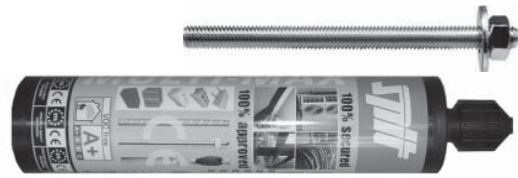
### $f_{\beta,V}$ INFLUENCE OF SHEAR LOADING DIRECTION

Angle $\beta$ [°]	$f_{\beta,V}$
0 to 55	1
60	1,1
70	1,2
80	1,5
90 to 180	2



# SPIT MULTI-MAX

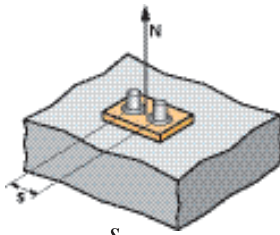
Zinc coated & stainless steel



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## SPIT CC- Method (values issued from ETA)

### $\Psi_s$ INFLUENCE OF SPACING FOR CONCRETE CONE RESISTANCE IN TENSILE LOAD



$$\Psi_s = 0,5 + \frac{s}{4 \cdot h_{ef}}$$

$S_{min} < S < S_{cr,N}$

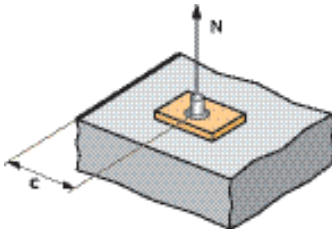
$S_{cr,N} = 2 \cdot h_{ef}$

$\Psi_s$  must be used for each spacing influenced the anchors group.

SPACING S	Reduction factor $\Psi_s$ Non-cracked concrete			
	M8	M10	M12	M16
40	0,58			
50	0,60	0,59		
60	0,63	0,61	0,59	0,58
80	0,67	0,65	0,62	0,61
100	0,71	0,69	0,65	0,63
150	0,81	0,78	0,73	0,70
200	0,92	0,87	0,80	0,77
250	1,00	0,96	0,88	0,83
300		1,00	0,95	0,90
330			1,00	0,94
375				1,00

SPACING S	Reduction factor $\Psi_s$ Non-cracked concrete	
	M20	M24
100	0,60	
120	0,62	0,60
150	0,65	0,62
180	0,68	0,64
200	0,70	0,66
250	0,75	0,70
350	0,84	0,78
450	0,94	0,86
510	1,00	0,90
630		1,00
750		1,00

### $\Psi_{c,N}$ INFLUENCE OF EDGE FOR CONCRETE CONE RESISTANCE IN TENSILE LOAD



$$\Psi_{c,N} = 0,27 + 0,725 \cdot \frac{c}{h_{ef}}$$

$C_{min} < C < C_{cr,N}$

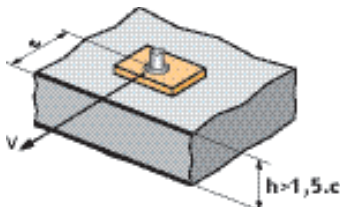
$C_{cr,N} = h_{ef}$

$\Psi_{c,N}$  must be used for each distance influenced the anchors group.

EDGE C	Reduction factor $\Psi_{c,N}$ Non-cracked concrete			
	M8	M10	M12	M16
40	0,50			
50	0,56	0,53		
60	0,63	0,58	0,52	
80	0,75	0,69	0,61	0,57
120	1,00	0,92	0,80	0,73
135		1,00	0,86	0,79
165			1,00	0,91
190				1,00

EDGE C	Reduction factor $\Psi_{c,N}$ Non-cracked concrete	
	M20	M24
100	0,54	
120	0,60	0,54
150	0,69	0,61
180	0,78	0,68
200	0,84	0,73
255	1,00	0,86
315		1,00

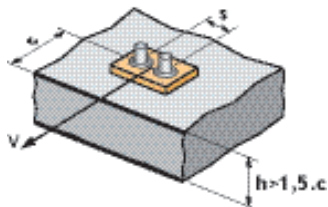
### $\Psi_{s-c,V}$ INFLUENCE OF SPACING AND EDGE DISTANCE FOR CONCRETE EDGE RESISTANCE IN SHEAR LOAD



$$\Psi_{s-c,V} = \frac{c}{c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$

For single anchor fastening

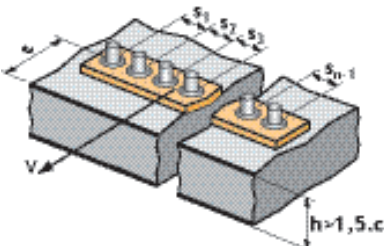
$\frac{c}{c_{min}}$	Factor $\Psi_{s-c,V}$ Non-cracked concrete												
	1,0	1,2	1,4	1,6	1,8	2,0	2,2	2,4	2,6	2,8	3,0	3,2	
$\Psi_{s-c,V}$	1,00	1,31	1,66	2,02	2,41	2,83	3,26	3,72	4,19	4,69	5,20	5,72	



$$\Psi_{s-c,V} = \frac{3 \cdot c + s}{6 \cdot c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$

For 2 anchors fastening

$\frac{c}{c_{min}}$	Factor $\Psi_{s-c,V}$ Non-cracked concrete												
	1,0	1,2	1,4	1,6	1,8	2,0	2,2	2,4	2,6	2,8	3,0	3,2	
1,0	0,67	0,84	1,03	1,22	1,43	1,65	1,88	2,12	2,36	2,62	2,89	3,16	
1,5	0,75	0,93	1,12	1,33	1,54	1,77	2,00	2,25	2,50	2,76	3,03	3,31	
2,0	0,83	1,02	1,22	1,43	1,65	1,89	2,12	2,38	2,63	2,90	3,18	3,46	
2,5	0,92	1,11	1,32	1,54	1,77	2,00	2,25	2,50	2,77	3,04	3,32	3,61	
3,0	1,00	1,20	1,42	1,64	1,88	2,12	2,37	2,63	2,90	3,18	3,46	3,76	
3,5		1,30	1,52	1,75	1,99	2,24	2,50	2,76	3,04	3,32	3,61	3,91	
4,0			1,62	1,86	2,10	2,36	2,62	2,89	3,17	3,46	3,75	4,05	
4,5				1,96	2,21	2,47	2,74	3,02	3,31	3,60	3,90	4,20	
5,0					2,33	2,59	2,87	3,15	3,44	3,74	4,04	4,35	
5,5						2,71	2,99	3,28	3,71	4,02	4,33	4,65	
6,0						2,83	3,11	3,41	3,71	4,02	4,33	4,65	



For 3 anchors fastening and more

$$\Psi_{s-c,V} = \frac{3 \cdot c + s_1 + s_2 + s_3 + \dots + s_{n-1}}{3 \cdot n \cdot c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$

# SPIT MULTI-MAX

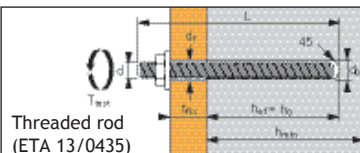
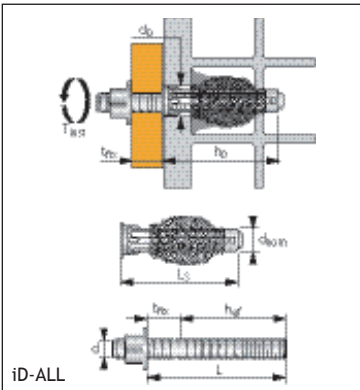
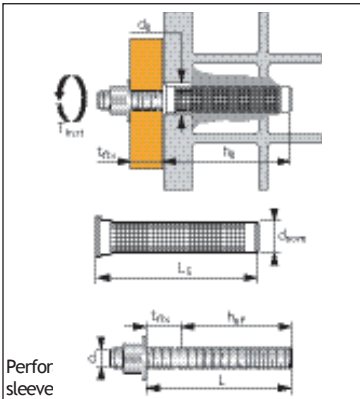


ETAG 029  
ETA n° 13/0437

## Methacrylate resin for fixing in hollow masonry

### Technical data

Type	Max. anchor depth (mm)	Max. thick of base material (mm)	Drilling depth (mm)	Ø thread (mm)	Ø Drill bit (mm)	Ø Clearance (mm)	Total rod length (mm)	Max. tighten (Nm)	Code
	$h_{ef}$	$d_o$	$h_o$	$d$	$L$	$d_{nom}$	$L_s$	$T_{inst}$	
iD-ALL + rod M8	65	16	70	8	$76 + t_{fix}$	16	70	3 <sup>(1)</sup>	-
iD-ALL + rod M10	65	16	70	10	$78 + t_{fix}$	16	70	3 <sup>(1)</sup>	-
Sleeve Ø20 + rod M12	85	20	90	12	$98 + t_{fix}$	20	85	3 <sup>(1)</sup>	061490
Sleeve Ø15 + rod M8	130	15	135	8	$138 + t_{fix}$	15	130	3 <sup>(1)</sup>	557080
Sleeve Ø15 + rod M10	130	15	135	10	$140 + t_{fix}$	15	130	3 <sup>(1)</sup>	557080
MULTI-MAX: Dual component cartridge methacrylate resin						- vol. 280 ml			060040
						- vol. 410 ml			060047



<sup>(1)</sup> 2 Nm in Clay masonry OPTIBRIC PV 3+ and in hollow concrete block.

### Working time and curing time

Ambient temperature (°C)	Working time	Curing time
30°C > T ≥ 40°C	2 min	35 min
20°C > T ≥ 30°C	4 min	45 min
10°C > T ≥ 20°C	6 min	60 min
5°C > T ≥ 10°C	12 min	90 min
0°C > T ≥ 5°C	18 min	180 min
-5°C > T ≥ 0°C	-	360 min

### Recommended loads in masonry with stud sleeve and iD-ALL (kN)

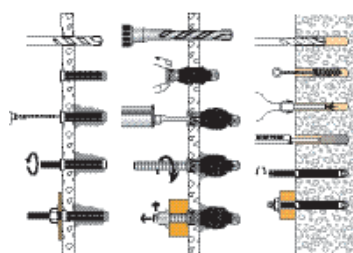
$$N_{Rec} = \frac{N_{Rk}}{\gamma_M \gamma_F}$$

$$V_{Rec} = \frac{V_{Rk}}{\gamma_M \gamma_F}$$

### APPLICATION

- Signs
- Scaffolding
- Electrical switchboards
- Radiators
- Air conditioning ducts
- Rail guard returns
- Blinds
- Climbing walls
- Metal scale
- Hand rails
- Pole and ducts
- Demountable partitions
- Kitchen furniture
- Decorations...

### INSTALLATION



Hollow material with sleeve    Hollow material with iD-ALL    Solid material

Type		Concrete hollow block B40		Clay masonry OPTIBRIC PV 3+		Clay masonry POROTHE RM GF R20 Th+		Clay masonry POROTHE RM R37 12-1,6-8 DF		Calcium silicate masonry KSL-R (P) 240	
		$f_b \geq 6.0$ N/mm <sup>2</sup>	$f_b \geq 9.0$ N/mm <sup>2</sup>	$f_b \geq 10.0$ N/mm <sup>2</sup>	$f_b \geq 8.0$ N/mm <sup>2</sup>	$f_b \geq 12.0$ N/mm <sup>2</sup>	$N_{rec}$	$V_{rec}$	$N_{rec}$	$V_{rec}$	
iD-ALL	M8	0.57	0.71	0.43	0.43	0.25	1.14	0.34	0.25	0.43	2.57
	M10										3.14
SLEEVE Ø20X85	M12	0.43	0.57	0.71	1.00	0.71	0.86	0.25	1.14	1.00	2.85
SLEEVE Ø15X130	M8	0.43	0.86	0.43	0.34	0.34	1.00	0.57	0.43	0.86	2.57
	M10										3.43

$\gamma_F = 1,4$  ;  $\gamma_M = 2,5$

# SPIT MULTI-MAX



## ▣ Rebar anchoring system



ETA - TR23  
n° 13/0436

### MULTI-MAX range

- Methacrylate resin
- Fast drying time
- Storage time: 18 months
- Usable in wet environments
- Styrene free
- V.O.C. (Volatile Organic Compounds) free
- Cartridge compatible with standard guns



## Range

### CARTRIDGES

- 060040 – Cartridge MULTI-MAX 280 ml (delivered with 2 injection nozzles)  
060047 – Cartridge MULTI-MAX 410 ml (delivered with 2 injection nozzles)

### INJECTION TOOLS

- 077151 – M380-410 manual injection tool  
050918 – P380-410 pneumatic injection tool  
054217 – EGI-380-410 electric injection tool  
063000 – M300 manual injection tool  
057912 – EGI-300 electric injection tool  
060052 – EGI battery

### CLEANING KITS

- 055832 – Manuel cleaning kit for rebar (without injection tool)  
055852 – Pneumatic cleaning kit for rebar (without injection tool)

### INJECTION NOZZLES

- 050882 – 150-300-345-380-410 10 nozzles

### NOZZLE EXTENSION TUBES

- 050898 – 8 x 200 extension for nozzles code 050882 & 050069  
050971 – 13 x 1000 extension for nozzles code 050882 & 050069  
063300 – 9 x 1000 extension for nozzles code 050882 & 050069  
050969 – Measuring caps (5 caps/package)



### METAL BRUSHES

- 052971 – Ø 11 metal brush  
052972 – Ø 13 metal brush  
052973 – Ø 15 metal brush  
052974 – Ø 20 metal brush  
052975 – Ø 22 metal brush  
052976 – Ø 26 metal brush  
052977 – Ø 30  
052978 – Ø 32 (to order)  
052979 – Ø 37 (to order)  
052981 – Ø 42 (to order)  
051010 – L325 metal brush extension  
051009 – L300 T-handle



### CLEANING BLOWER

- 065990 – Manual cleaning blower





ETA - TR 023  
n° 13/0436

## METHACRYLATE RESIN

### Steel reinforcement fixings for reinforced concrete



#### Mechanical Characteristics of rebars

Nominal steel bar Ø		8	10	12	14	16	20
Sections (cm <sup>2</sup> )		0.503	0.785	1.13	1.54	2.01	3.14
Min. resistances to failure (kN)	Fe E400	21,13	32,97	47,46	64,68	84,42	131,88
	Fe E500	25,90	40,43	58,20	79,31	103,52	161,71
Ultimate limit load N <sub>Rd</sub> (kN)	Fe E500	21,85	34,15	49,17	66,93	87,42	136,59

The mechanical characteristics of the high adhesion rebars are defined in the NFA 35-016 and NFA 35-017.

#### SIZING RULES FOR STEEL REINFORCEMENT FIXINGS FOR CONCRETE ACCORDING TO EUROCODE 2 REGULATIONS AND ETA 13/0436

The basic anchorage length  $L_{b,rqd}$  (mm) for the ultimate limit load for rebar  $F_{Rd}$  (N) is given by following equation:

$$L_{b,rqd} = \frac{F_{Rd}}{\Pi \cdot \varnothing \cdot \eta_1 \cdot \eta_2 \cdot f_{bd}}$$

$F_{Rd}$  : Design ultimate load (N))

$f_{bd}$  : Design value of the bond strength in N/m<sup>2</sup>  
d'adhérence en N/mm<sup>2</sup>

$\varnothing$  : Rebar diameter (mm)

$\eta_1$  : depends on bond conditions -  $\eta_1 = 1$  (good bond conditions). See § 8.4.2 (EN 1992-1-1)

$\eta_2$  : depends on rebar diameter -  $\eta_2 = 1$  for  $\varnothing_{bar} \leq 32$  mm

The design anchorage length  $L_{bd}$  (mm) is determined as follow:

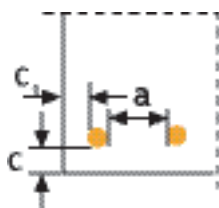
$$L_{bd} = L_{b,rqd} \cdot \alpha_2 \cdot \alpha_5$$

Size	f <sub>bd</sub> Design adhesive strength according to EN 1992-1-1								
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
Ø8	1.6	2.0	2.3	2.7	3.0	3.4	3.4	3.7	3.7
Ø10	1.6	2.0	2.3	2.7	3.0	3.4	3.4	3.4	3.4
Ø12	1.6	2.0	2.3	2.7	3.0	3.0	3.0	3.0	3.4
Ø14	1.6	2.0	2.3	2.7	3.0	3.0	3.0	3.0	3.0
Ø16	1.6	2.0	2.3	2.7	2.7	2.7	2.7	2.7	3.0
Ø20	1.6	2.0	2.3	2.3	2.3	2.3	2.3	2.3	2.7

With  $\alpha_2$  : Influence of concrete minimum cover.

$$\alpha_2 = 1 - 0.15(Cd - \varnothing_{fer}) / \varnothing_{fer} \geq 0,7$$

$$Cd = \min\left(c; c_1; \frac{a}{2}\right)$$



With  $\alpha_5$  : Influence of the confinement by transverse pressure.

The factor  $\alpha_5$  take into account of the effect of the pressure transverse to the plane of splitting along the design length.

$$\alpha_5 = 1 - 0,04 \cdot p \geq 0,7$$

p (Mpa)	$\alpha_5$
3	0,88
5	0,8
7	0,72

where  $p$  is the transverse pressure at the ultimate limit state along  $L_{bd}$  in MPa.

#### Limit of this formula

- The max. anchor depth will be limited to 900 mm with pneumatic injection tool.

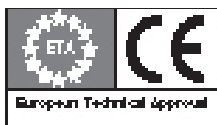
# SPIT MULTI-MAX



## Eurocode 2 table for straight rebar anchoring



### CONCRETE C25/30 - HAMMER DRILLING



ETA 13/0436



Rebar Ø (mm)	Drilling Ø d <sub>0</sub> (mm)	Length of anchor L <sub>bd</sub> (mm)	Ultimate limit load (daN) <u>without influence</u> of centre distance and/or edge <sup>(1)</sup> (α <sub>2</sub> = 0,7)	Ultimate limit load (daN) <u>with influence</u> of centre distance and/or edge <sup>(2)</sup> (α <sub>2</sub> = 1)	Number of fixings for a SPIT MULTI-MAX cartridge <sup>(3)</sup>	
					280 ml	410 ml
8	10	170	1648	1154	48,5	71,1
		190	1842	1289	43,4	63,6
		225	2185	1530	36,6	53,6
		322	-	2185	25,6	37,5
10	12	213	2577	1804	31,7	46,5
		240	2908	2036	28,1	41,2
		282	3415	2391	24,0	35,1
		403	-	3415	16,8	24,6
12	15	255	3711	2597	14,4	21,0
		290	4217	2952	12,6	18,5
		338	4917	3442	10,8	15,9
		483	-	4917	7,6	11,1
14	18	298	5051	3536	7,8	11,4
		340	5768	4038	6,8	10,0
		395	6693	4685	5,9	8,6
		564	-	6693	4,1	6,0
16	20	340	6597	4618	6,1	8,9
		380	7367	5157	5,4	7,9
		451	8742	6119	4,6	6,7
		644	-	8742	3,2	4,7
20	25	425	8781	6147	3,1	4,5
		490	10116	7081	2,7	3,9
		662	13659	9561	2,0	2,9
		900	-	13006	1,5	2,1

(1) Absence of edge distances greater than or equal to 7.Ø.

(2) Presence of edge distances and/or centre distances less than 7.Ø.

(3) The number of fixings per cartridge is calculated taking into account an increasing by 20% the real volume of sealing.  
 $1,2 \times (d_0^2 - \varnothing_{\text{rebar}}^2) \times \Pi \times L_{bd} / 4$